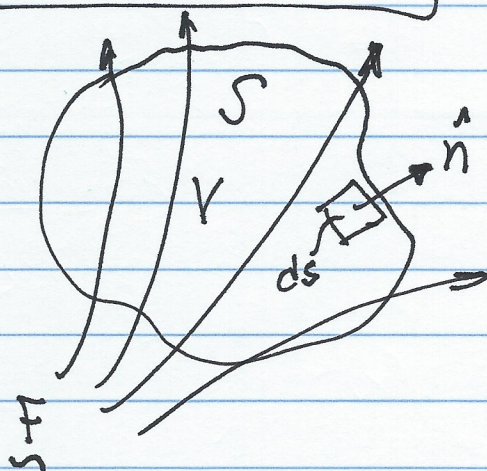


14.8 THE DIVERGENCE THEOREM (GAUSS' THEOREM)

$$\int_V \nabla \cdot \underline{F} dV = \oint_S \underline{F} \cdot d\underline{S}$$

S is the closed surface, enclosing V
 $\hat{n}$ is the outward normal

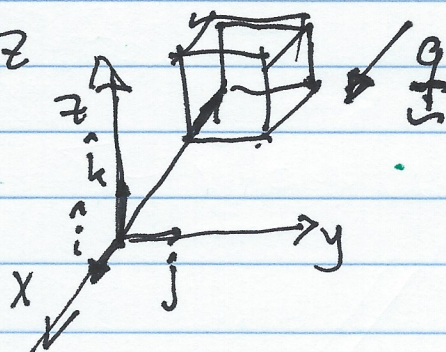
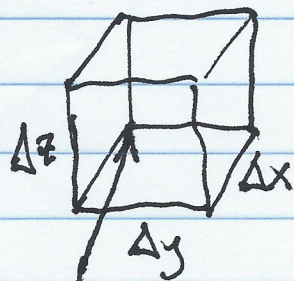


To get some intuition, look at simplest possible problem:

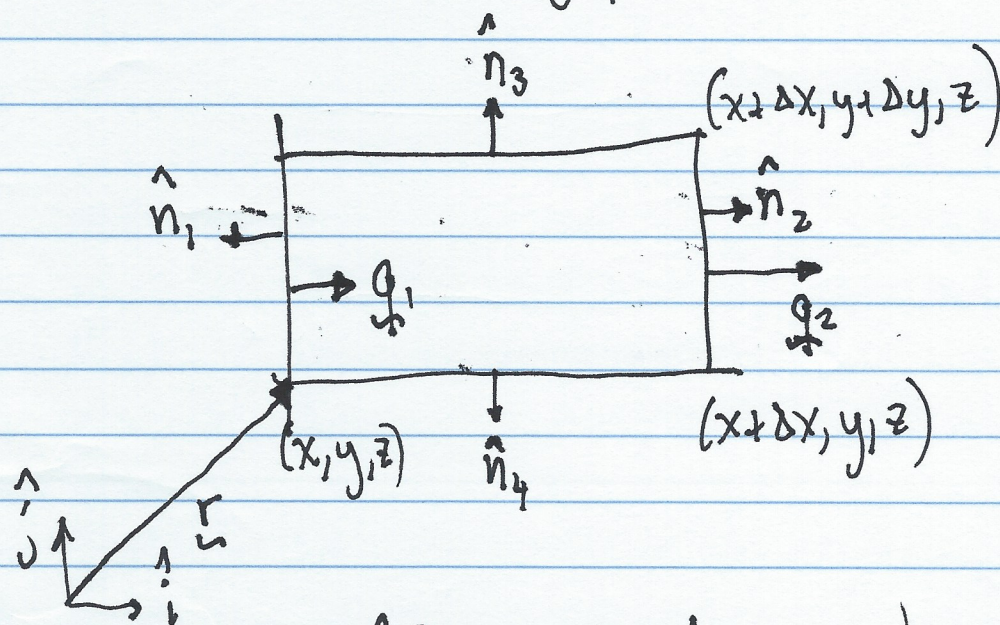
$$\text{let } \underline{g} = \hat{i} f(x)$$

V is going to be a box located at (x, y, z)

and size $\Delta x \times \Delta y \times \Delta z$



Side View in xy plane



$$\left\{ \begin{array}{ll} q_1 = \hat{i} f(x) & \hat{n}_1 = -\hat{i} \\ q_2 = \hat{i} f(x+\Delta x) & \hat{n}_2 = \hat{i} \end{array} \right. \quad \left\{ \begin{array}{ll} \hat{n}_3 = \hat{j} & q_3 = \hat{j} f(y) \\ \hat{n}_4 = -\hat{j} & q_4 = -\hat{j} f(y) \end{array} \right.$$

Let's compute ^{total} ~~differences~~ of fluxes entering & exiting the box:

$$q_2 \cdot \hat{n}_2 dy dz + q_1 \cdot \hat{n}_1 dy dz$$

(no fluxes entering/leaving in the y direction because $q = f(x)\hat{i}$, i.e. aligned in the x direction)

$$\begin{aligned} & [f(x+\Delta x)\hat{i} \cdot \hat{i} - f(x)\hat{i} \cdot \hat{i}] dy dz \\ & = [f(x+\Delta x) - f(x)] dy dz \end{aligned}$$

$$\text{but } f(x+\Delta x) \approx f(x) + \Delta x \frac{df}{dx} + \frac{1}{2} \Delta x^2 \frac{d^2f}{dx^2} + \dots$$

$$\therefore [f(x+\Delta x) - f(x)] dy dz$$

$$= [f(x) + \Delta x f' + \frac{1}{2} \Delta x^2 f'' + \dots - f(x)] dy dz$$

if $|\Delta x| \ll 1$ then

$$\approx \left[f(x) + \Delta x \frac{df}{dx} - f(x) \right] dy dz$$

$$= \frac{df}{dx} \Delta x dy dz = \frac{df}{dx} dx dy dz = \frac{df}{dx} dV$$

More generally, suppose $\underline{\underline{q}} = f(x, y) \hat{i} + g(x, y) \hat{j}$

The total fluxes entering/leaving box is what's entering & leaving sides 1 & 2, which is,

$$\frac{\partial f(x, y)}{\partial x} dV$$

plus how much enters/leaves sides 3 and 4:

$$(\underline{\underline{q}}_3 \cdot \hat{n}_3 + \underline{\underline{q}}_4 \cdot \hat{n}_4) dx dz = [g(x, y+\Delta y) - g(x, y)] dx dz$$

$$\approx \frac{\partial g}{\partial y} dy dx dz = \frac{\partial g}{\partial y} dV$$

Consider the most general case:

$$\underline{q} = f(x,y,z)\hat{i} + g(x,y,z)\hat{j} + h(x,y,z)\hat{k}$$

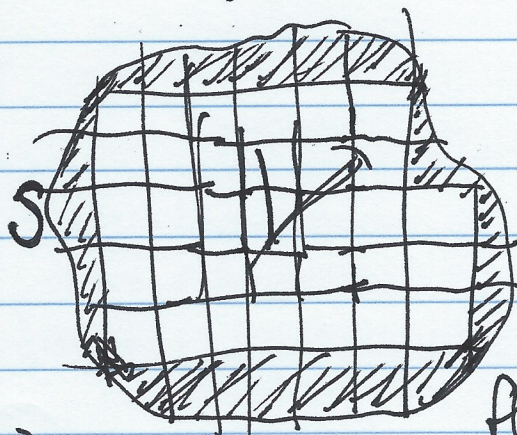
Total fluxes will be $\left[\frac{\partial f}{\partial x} + \frac{\partial g}{\partial y} + \frac{\partial h}{\partial z} \right] dV$

$$= \underline{q} \cdot \hat{n} dS$$

Integrating over a volume enclosed by S :

$$\int_V (\nabla \cdot \underline{q}) dV = \oint_S \underline{q} \cdot \hat{n} dS \quad dS = \hat{n} dS //$$

Another way to make sense of this:



Take a closed volume and grid up its interior. In each of the boxes compute the total fluxes. Add all these fluxes. Since any net (positive/negative) flux from one box is taken

~~(in/out)~~ (in/out) by neighbor boxes, their total sum would zero out, EXCEPT for boxes near the surface S . Hence

Sum fluxes = Sum of fluxes of outer boxes, the shaded ones.

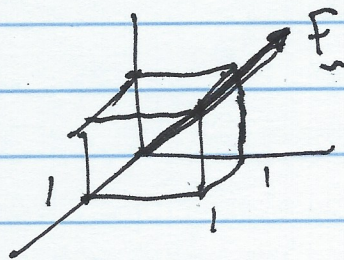
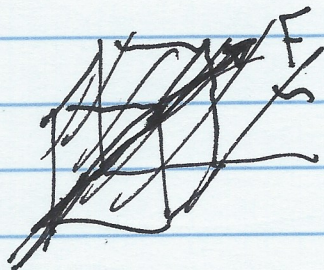
We saw that each box contributes
 $(\nabla \cdot \vec{F})_i dV_i$ fluxes so

sum of these must equal to the net
 fluxes leaving the volume

ex) Verify the divergence theorem

$$\vec{F} = x\hat{i} + y\hat{j} + z\hat{k}$$

For a surface of a cube bounded by the coordinate
 planes and the planes $x=1, y=1, z=1$:

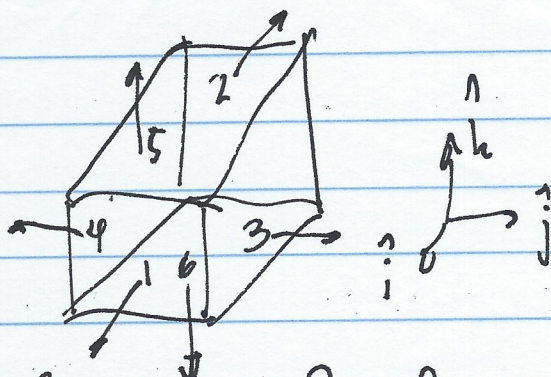


V has volume of 1.

$$\int_V \nabla \cdot \vec{F} dV = \oint_S \vec{F} \cdot \hat{n} dS$$

$$\nabla \cdot \vec{F} = \nabla \cdot (x\hat{i} + y\hat{j} + z\hat{k}) = 3 \quad \therefore \int_V \nabla \cdot \vec{F} dV = 3 \int_V dV = 3$$

$$\text{Now } \oint_S \vec{F} \cdot \hat{n} dS = \int_{S_1} + \int_{S_2} + \int_{S_3} + \int_{S_4} + \int_{S_5} + \int_{S_6}$$



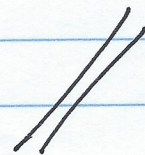
$$\oint_S \mathbf{F} \cdot \hat{\mathbf{n}} dS = \underbrace{\int_{S_1} + \int_{S_2}} + \underbrace{\int_{S_3} + \int_{S_4}} + \underbrace{\int_{S_5} + \int_{S_6}}$$

$$\int_{S_1+S_2} = \iint_{S_1} \mathbf{F} \cdot \hat{\mathbf{i}} dy dz + \iint_{S_2} \mathbf{F} \cdot (-\hat{\mathbf{i}}) dy dz = \iint x|_1 dy dz - \iint 0 dy dz = 1$$

$$\int_{S_3+S_4} = \iint y|_{y=1} dx dz - \iint 0 dx dz = 1$$

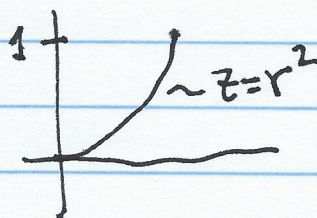
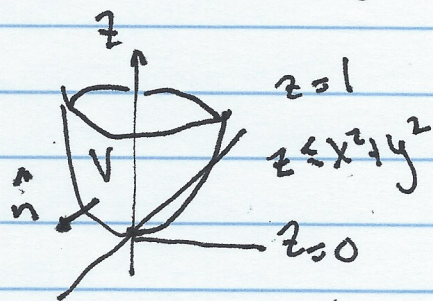
$$\int_{S_5+S_6} = 1$$

$$\therefore \oint_S \mathbf{F} \cdot \hat{\mathbf{n}} dS = 3$$



ex) Verify the divergence theorem

$$\underline{E} = \frac{1}{2}y\hat{i} + \frac{1}{2}x\hat{j} + z^2\hat{k}$$



$$\int_V (\nabla \cdot \underline{E}) dV = \oint_S \underline{E} \cdot d\underline{S}$$

$$\hookrightarrow \nabla \cdot \underline{E} = 2z$$

$$\iiint_V 2z dx dy dz = 2 \int_0^{2\pi} d\theta \int_0^1 dr r \int_{r^2}^1 z dz = 4\pi \int_0^1 dr r \left. \frac{1}{2} z^2 \right|_{r^2}^1$$

$$= \frac{4\pi}{2} \int_0^1 dr r (1 - r^4) = 2\pi \int_0^1 dr (r - r^5) = 2\pi \left(\frac{1}{2} r^2 - \frac{1}{6} r^6 \right) \Big|_0^1$$

$$= 2\pi \left(\frac{1}{2} - \frac{1}{6} \right) = \frac{2\pi}{3}$$

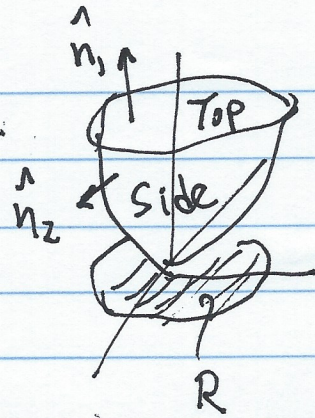
Now, let's do

$$\oint_S \underline{E} \cdot d\underline{S} = \int_{\text{Top}} + \int_{\text{Side}}$$

$$\text{Top: } \int_{\text{Top}} \underline{E} \cdot \hat{n}_1 dS_1$$

$$\hat{n}_1 = \hat{k} \quad dS_1 = dx dy$$

$$\int_{\text{Top}} z^2 dx dy = \iint_{\text{Top}} dx dy = \pi$$



$$\text{Side: let } g = -z + x^2 + y^2 \quad \hat{n}_2 = \frac{\nabla g}{|\nabla g|} = \frac{-\hat{k} + 2x\hat{i} + 2y\hat{j}}{\sqrt{1 + 2x^2 + 2y^2}}$$

$$\int_{\text{side}} \underline{E} \cdot \hat{n}_2 dS_2 = \iint_R \underline{E} \cdot \hat{n}_2 \frac{dx dy}{|\hat{n}_2 \cdot \hat{k}|} = \iint_R \left(\frac{1}{2}y\hat{i} + \frac{1}{2}x\hat{j} + z\hat{k} \right) \cdot \hat{n}_2 \frac{dx dy}{|\hat{n}_2 \cdot \hat{k}|}$$

$$\hat{n}_2 \cdot \hat{k} = \frac{-1}{|\nabla g|} \quad \therefore \frac{\hat{n}_2}{|\hat{n}_2 \cdot \hat{k}|} = |\nabla g| \hat{n}_2 = |\nabla g| \frac{\nabla g}{|\nabla g|} = \nabla g$$

$$\iint_R \left(\frac{1}{2}y\hat{i} + \frac{1}{2}x\hat{j} + z\hat{k} \right) \cdot (2x\hat{i} + 2y\hat{j} - \hat{k}) dx dy = \iint_R (xy + xy - z^2) dx dy$$

$$\begin{aligned} \text{but } z = r^2 \therefore 2r^2 \sin\theta \cos\theta - r^4 &= 2xy - z^2 \\ \int_0^{2\pi} \int_0^1 r dr (2r^2 \sin\theta \cos\theta - r^4) &= \int_0^{2\pi} d\theta \left[\frac{2}{3} r^3 \sin\theta \cos\theta - \frac{1}{5} r^5 \right]_0^1 \\ &= \int_0^{2\pi} d\theta \left[\frac{2}{3} \sin\theta \cos\theta - \frac{1}{5} \right] = \int_0^{2\pi} \frac{1}{3} \frac{d}{d\theta} [\sin^2\theta] d\theta - \frac{1}{5} 2\pi = -\frac{2}{5}\pi \end{aligned}$$

Note:

$$\left[\frac{1}{3} \sin^2 \theta \right]_0^{2\pi} = 0$$

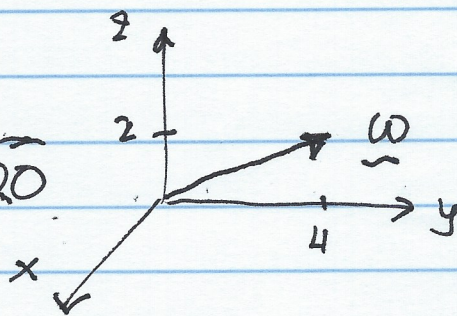
$$\therefore \int_{\text{Top side}} + \int = \pi - \frac{1}{3}\pi = \frac{2\pi}{3} \text{ which agrees with the } \int_V \nabla \cdot \underline{E} dV \text{ result}$$

ex) A rotating field $\underline{V} = \langle 2z - y, x, -2x \rangle$

"rotating" because its curl is not zero:

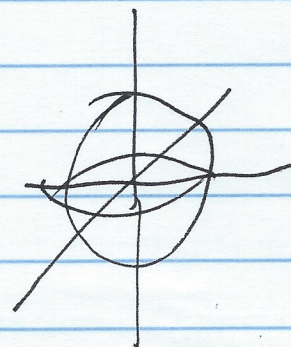
$$\underline{\omega} = \nabla \times \underline{V} = 4\hat{j} + 2\hat{k}$$

The rotation rate $|\underline{\omega}| = \sqrt{4^2 + 2^2} = \sqrt{20}$



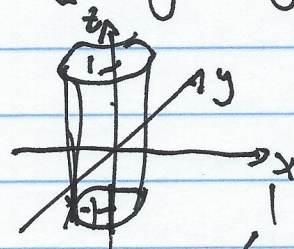
Find total flux in a unit ball center at the origin.

$$\oint_S \underline{V} \cdot \hat{n} dS = \int_V \nabla \cdot \underline{V} dV$$



ex) Verify $\int_V \nabla \cdot \underline{F} dV = \oint_S \underline{F} \cdot d\underline{S}$ where $\underline{F} = xy^2 \hat{i} + x^2y \hat{j} + y \hat{k}$

for a cylinder $-1 \leq z \leq 1$ $x^2 + y^2 = 1$



$$\nabla \cdot \underline{F} = x^2 + y^2 = r^2$$

$$\int_V (x^2 + y^2) dx dy dz = \int_{-1}^1 dz \int_0^{2\pi} d\theta \int_0^1 r dr r^2 = 2 \cdot 2\pi \int_0^1 r^3 dr = 2 \cdot 2\pi \frac{1}{4} = \pi //$$

$$\oint_S \underline{F} \cdot d\underline{S} = \int_{\text{top}} + \int_{\text{bottom}} + \int_{\text{side}}$$

$$\int_{\text{top}} + \int_{\text{bottom}} = \int_{S_{\text{top}}} \underline{F} \cdot \hat{n}_{\text{top}} dx dy + \int_{S_{\text{bottom}}} \underline{F} \cdot \hat{n}_{\text{bottom}} dx dy = \int_{S_{\text{top}}} y \hat{k} \cdot \hat{k} dx dy + \int_{S_{\text{bottom}}} y \hat{k} \cdot (-\hat{k}) dx dy = 0$$

For the side $\hat{n} = \hat{r}$ and $dS = dz d\theta$; $F(x, y, z)$ needs to be expressed in cylindrical coordinates

$$\hat{i} = \cos\theta \hat{r} - \sin\theta \hat{\theta} \quad \hat{j} = \sin\theta \hat{r} + \cos\theta \hat{\theta} \quad \hat{k} = \hat{k}$$

Since $\underline{F} \cdot \hat{r} dS$ only has a contribution from $\hat{r}$, ignore all terms in the $\hat{\theta}$ and $\hat{k}$ direction

$$\underline{F} = r^3 \cos\theta \sin^2\theta (\cos\theta \hat{r} - \sin\theta \hat{\theta}) + r^3 \cos^2\theta \sin\theta (\sin\theta \hat{r} + \cos\theta \hat{\theta}) + r \sin\theta \hat{k}$$

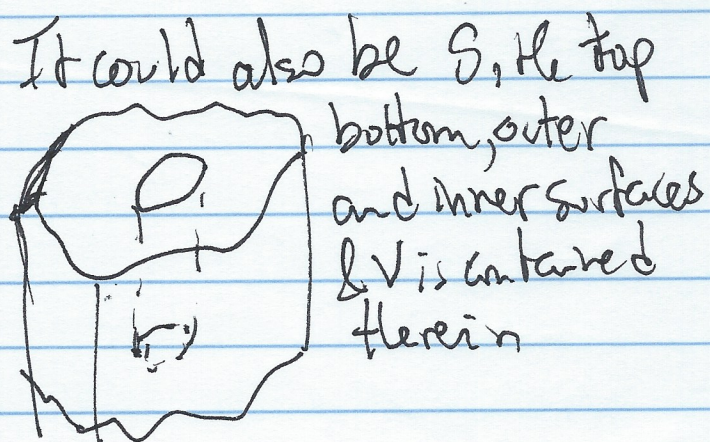
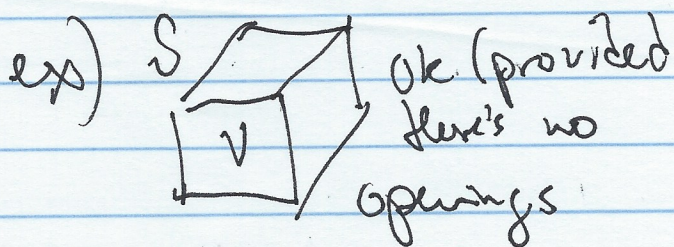
$$\underline{F} \cdot \hat{r} = r^3 \cos^2\theta \sin^2\theta + r^3 \cos^2\theta \sin^2\theta = 2 r^3 \cos^2\theta \sin^2\theta$$

$$= \frac{1}{2} r^3 (1 + \cos 2\theta)(1 - \cos 2\theta) = \frac{1}{2} r^3 \sin^2 2\theta$$

$$\therefore \int_{\text{side}} \underline{F} \cdot \hat{n} dS = \int_{-1}^1 dz \int_0^{2\pi} \frac{1}{2} r^3 \big|_{r=1} \sin^2 2\theta d\theta = \int_0^{2\pi} \sin^2 2\theta d\theta$$

$$= \int_0^{2\pi} d\theta \frac{1}{2} (1 - \cos 4\theta) = \int_0^{2\pi} d\theta \frac{1}{2} = \pi //$$

S must be closed and continuous, so



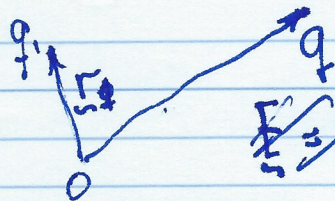
What about $\vec{F}$? it must be continuous and its $\nabla \cdot \vec{F}$ must be defined everywhere inside S . It must be defined on S .

So obviously, sometimes the choice of S, V is given by the application, sometimes by the region whereby $\vec{F}$ has the right properties.

Let's see how this plays out. It leads to "Gauss' Law"

Gauss' Law

$$\oint \mathbf{E} \cdot \mathbf{\hat{n}} d\phi = \frac{q}{\epsilon_0}$$



~~$$\mathbf{E} = k \frac{q}{r^2} \mathbf{\hat{r}}$$~~

$$\mathbf{E} = \frac{q}{4\pi\epsilon_0} \frac{(\mathbf{r} - \mathbf{r}_i)}{|\mathbf{r} - \mathbf{r}_i|^3}$$

Electricity: (Plate with infinity)

$$\mathbf{E} = \frac{q}{4\pi\epsilon_0} \frac{\mathbf{r}}{r^3}$$

field due to a point charge (at origin)

permittivity (of free space)

Find the flux of this point charge at any surface enclosing it.

$$\oint_S \mathbf{E} \cdot \mathbf{\hat{n}} d\phi = \int_V \nabla \cdot \mathbf{E} dV$$

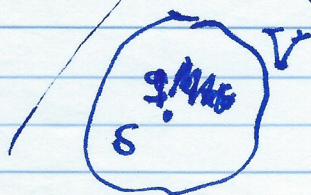
since $\mathbf{r} = x\mathbf{\hat{i}} + y\mathbf{\hat{j}} + z\mathbf{\hat{k}}$

$$\nabla \cdot \mathbf{E} = \frac{q}{4\pi\epsilon_0} \left[\frac{\partial}{\partial x} \left(\frac{x}{r^3} \right) + \frac{\partial}{\partial y} \left(\frac{y}{r^3} \right) + \frac{\partial}{\partial z} \left(\frac{z}{r^3} \right) \right]$$

$$\begin{aligned} \frac{\partial}{\partial x} \left(x [x^2 + y^2 + z^2]^{-3/2} \right) &= [x^2 + y^2 + z^2]^{-3/2} - \frac{3}{2} x [x^2 + y^2 + z^2]^{-5/2} (2x) \\ &= r^{-3} - 3x^2 r^{-5} \end{aligned}$$

$$\therefore \nabla \cdot \left(\frac{\mathbf{r}}{r^3} \right) = 3r^{-3} - 3(x^2 + y^2 + z^2) r^{-5} = 0$$

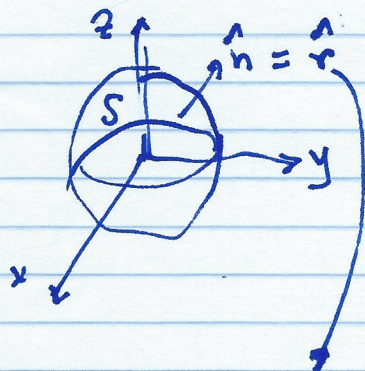
~~$$\therefore \oint_S \mathbf{E} \cdot \mathbf{\hat{n}} dS = 0 \text{ regardless of shape of } S \text{ so long as it encloses } V.$$~~

Wrong!Why??

Note that $\frac{\underline{r}}{|\underline{r}|^3}$ is not defined at origin!!
 $\therefore \nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right)$ is not defined either!

New Calculation

Find the flux (we'll use a sphere)
 the general case is technically involved



$$\oint_S \underline{E} \cdot \hat{n} d\phi$$

$$= \frac{Q}{4\pi\epsilon_0} \int \frac{\underline{r}}{|\underline{r}|^3} \cdot \frac{\underline{r}}{|\underline{r}|} d\phi = \frac{Q}{4\pi\epsilon_0} \int \frac{|\underline{r}|^2}{|\underline{r}|^4} d\phi = \frac{Q}{4\pi\epsilon_0 a^2} \int d\phi$$

Sphere

$$= \frac{Q}{4\pi\epsilon_0 a^2} 4\pi a^2 = \frac{Q}{\epsilon_0}$$

Generally.

$$\text{so } \oint_S \underline{E} \cdot \hat{n} d\phi = \frac{Q}{\epsilon_0} = \frac{1}{\epsilon_0} \int_V \rho dV$$

Total charge

//
~~Let's try~~ So we have

~~$$\int \nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right) dV$$~~

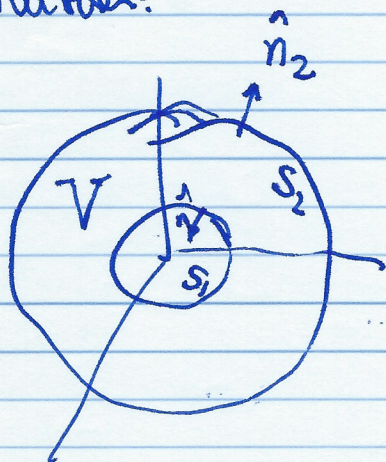
$$\nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right) = 0 \text{ true if } \underline{r} \neq \underline{0} \text{ (exclude the origin)}$$

8

$$\int_V \nabla \cdot \underline{E} dV = \oint_S \underline{E} \cdot \hat{n} d\sigma = \frac{Q}{\epsilon_0}$$

this can't be 0 and Q/ϵ_0 at the same time!

The solution:



Now

$$\nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right) = 0$$

since the origin is not included

$$\int_V \nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right) dV = 0$$

$$\frac{Q}{4\pi\epsilon_0} \int_V \nabla \cdot \left(\frac{\underline{r}}{|\underline{r}|^3} \right) dV = 0 = \int_{S_1} \underline{E} \cdot \hat{n}_1 d\sigma + \int_{S_2} \underline{E} \cdot \hat{n}_2 d\sigma$$

$$\text{but } \int_{S_2} \underline{E} \cdot \hat{n}_2 d\sigma = \frac{Q}{\epsilon_0} \Rightarrow \int_{S_1} \underline{E} \cdot \hat{n}_1 d\sigma = -\frac{Q}{\epsilon_0}$$